# A STUDY OF GREEN'S FUNCTIONS FOR TWO-DIMENSIONAL PROBLEM IN ORTHOTROPIC MAGNETOTHERMOELASTIC MEDIA WITH MASS DIFFUSION

Rajneesh Kumar<sup>\*</sup>, Vijay Chawla<sup>\*\*</sup>

Department of Mathematics, Kurukshetra University, Kurukshetra, 136119, Haryana, India \*e-mail: rajneesh kuk@rediffmail.com

\*\*e-mail: vijay1 kuk@rediffmail.com

**Abstract.** The present investigation deals with the study of Green's functions for twodimensional problem in orthotropic magnetothermoelastic media with mass diffusion. After applying the dimensionless quantities and using the operator theory, two-dimensional general solution in orthotropic magnetothermoelastic diffusion media is derived. On the basis of general solution, the Green's functions for a steady line on the surface of a semi-infinite orthotropic magnetothermoelastic diffusion material are constructed by four newly introduced harmonic functions. The components of displacement, stress, temperature distribution and mass concentration are expressed in terms of elementary functions. From the present investigation, some special cases of interest are also deduced and compared with the previous results obtained. The resulting quantities are computed numerically for semi-infinite magneto thermoelastic material and presented graphically to depict the effect of magnetic.

#### **1. Introduction**

Fundamental solutions or Green's functions play an important role in both applied and theoretical studied on the physics of solids. Fundamental solutions can be used to construct many analytical solutions solving boundary value problems of practical problems when boundary conditions are imposed. They are essential in boundary element method (BEM) as well as the study of cracks, defects and inclusion. Many researchers have been investigated the Green's function for elastic solid in isotropic and anisotropic elastic media, notable among them are Freedholm [1], Lifshitz and Rezentsveig [2], Elliott [3], Kröner [4], Synge [5], Lejcek [6], Pan and Chou [7], and Pan and Yuan [8].

When thermal effects are considered, Sharma [9] investigated the fundamental solution for transversely isotropic thermoelastic material in an integral form. Chen et al. [10] derived the three dimensional general solution for transversely isotropic thermoelastic materials. Hou et al. [11, 12] investigated the Green's function for two and three-dimensional problem for a steady Point heat source in the interior of a semi-infinite thermoelastic materials. Also, Hou et.al [13] investigated the two dimensional general solutions and fundamental solutions for orthotropic thermoelastic materials.

The theory of magnetothermoelasticity is concerned with the interacting effects of the applied magnetic field on the elastic and thermoelastic deformation of a solid body. This theory has drawn the attention of many researchers because of its extensive uses in diverse fields, such as geophysics for understanding the effect of Earth's magnetic field on seismic waves, damping of acoustic waves in a magnetic field. Kolaski and Nowacki [14] studied the magnetothermoelastic disturbance in a perfectly conducting elastic half-space in contact with

# (i) Constitutive relations:

80

$$\sigma_{ij} = c_{ijkm} \varepsilon_{km} + a_{ij} \mathbf{T} + b_{ij} C, \tag{5}$$

# (ii) Equations of motion:

$$c_{ijkm}e_{km,j} + a_{ij}T_{,j} + b_{ij}C_{,j} + F_i = \rho \ddot{u}_i,$$
(6)

#### (iii) Equation of heat conduction:

$$\rho C_E \dot{\mathbf{T}} + a \mathbf{T}_0 \dot{C} - a_{ij} \mathbf{T}_0 \dot{\varepsilon}_{ij} = K_{ij} \mathbf{T}_{,ij},\tag{7}$$

### (iv) Equation of mass diffusion:

$$-\alpha_{ij}^{*}b_{km}\varepsilon_{km,ij} - \alpha_{ij}^{*}bC_{,ij} + \alpha_{ij}^{*}aT_{,ij} = -\dot{C}.$$
(8)

Here,  $c_{ijkm} (= c_{kmij} = c_{jikm} = c_{ijmk})$  are elastic parameters,  $a_{ij} (= a_{ji})$ ,  $b_{ij} (= b_{ji})$  are, respectively, the tensors of thermal and diffusion modules,  $\rho$  is the density and  $C_E$  is the specific heat at constant strain, a,b are, respectively, coefficients describing the measure of thermoelastic diffusion effects and diffusion effects,  $T_0$  is the reference temperature assumed to be such that

$$\left|\frac{T}{T_0}\right| \ll 1, K_{ij}(=K_{ji}), \sigma_{ij}(=\sigma_{ji}) \text{ and } \varepsilon_{ij} = \frac{u_{i,j} + u_{j,i}}{2} \text{ denote the components of thermal}$$

conductivity, stress and strain tensor respectively, T(x, y, z, t) is the temperature change from the reference temperature  $T_0$  and C is the mass concentration,  $u_i$  are components of displacement vector,  $\alpha_{ii}^* (= \alpha_{ii}^*)$  are diffusion parameters,  $F_i$  are components of Lorentz force.

In the above equations symbol (",") followed by a suffix denotes differentiation with respect to spatial coordinate and a superposed dot (".") denotes the derivative with respect to time respectively.

#### 3. Formulation of the problem

We consider homogenous orthotropic magnetothermoelastic diffusion medium. Let us take Oxyz as the frame of reference in Cartesian coordinates, the origin O being any point on the plane boundary.

For two-dimensional problem, we assume the displacement vector, temperature change and mass concentration are, respectively, of the form

$$\mathbf{u} = (u, 0, w),$$
  $T(x, z, t),$   $C(x, z, t),$  (9)

and Lorentz force is taken in the form (for two dimensional problem):

$$F_1 = \mu_0 H_0^2 \left(\frac{\partial e}{\partial x} - \varepsilon_0 \mu_0 \frac{\partial^2 u}{\partial t^2}\right),\tag{10a}$$

$$F_3 = \mu_0 H_0^2 \left(\frac{\partial e}{\partial z} - \varepsilon_0 \mu_0 \frac{\partial^2 w}{\partial t^2}\right), \tag{10b}$$

$$\varepsilon_{2} = \frac{a_{3}}{a_{1}}, \qquad \varepsilon_{3} = \frac{K_{3}}{K_{1}}, \quad (q_{1}^{*}, q_{2}^{*}) = \frac{\alpha_{1}^{*}\omega_{1}^{*}}{c_{11}}(b_{1}, b_{3}), \qquad (q_{3}^{*}, q_{4}^{*}) = \frac{\alpha_{3}^{*}\omega_{1}^{*}}{c_{11}}(b_{1}, b_{3}),$$
$$(q_{5}^{*}, q_{6}^{*}) = \frac{\omega_{1}^{*}b}{b_{1}}(\alpha_{1}^{*}, \alpha_{3}^{*}), \qquad (q_{7}^{*}, q_{8}^{*}) = \frac{a\omega_{1}^{*}}{a_{1}}(\alpha_{1}^{*}, \alpha_{3}^{*}).$$

The equations (13)-(16) can be written as

$$D\{u, w, C, T\}^{t} = 0.$$
(17)

where D is differential operator matrix given by

$$\begin{bmatrix} \delta_{1} \frac{\partial^{2}}{\partial x^{2}} + \delta_{2} \frac{\partial^{2}}{\partial z^{2}} & \delta_{3} \frac{\partial^{2}}{\partial x \partial z} & -\frac{\partial}{\partial x} & -\frac{\partial}{\partial x} \\ \delta_{3} \frac{\partial^{2}}{\partial x \partial z} & \delta_{2} \frac{\partial^{2}}{\partial x^{2}} + \delta_{4} \frac{\partial^{2}}{\partial z^{2}} & -\varepsilon_{1} \frac{\partial}{\partial z} & -\varepsilon_{2} \frac{\partial}{\partial z} \\ \frac{\partial}{\partial x} \left( q_{1}^{*} \frac{\partial^{2}}{\partial x^{2}} + q_{3}^{*} \frac{\partial^{2}}{\partial z^{2}} \right) & \frac{\partial}{\partial z} \left( q_{2}^{*} \frac{\partial^{2}}{\partial x^{2}} + q_{4}^{*} \frac{\partial^{2}}{\partial z^{2}} \right) & - \left( q_{5}^{*} \frac{\partial^{2}}{\partial x^{2}} + q_{6}^{*} \frac{\partial^{2}}{\partial x^{2}} \right) & \left( q_{7}^{*} \frac{\partial^{2}}{\partial x^{2}} + q_{8}^{*} \frac{\partial^{2}}{\partial x^{2}} \right) \\ 0 & 0 & 0 & \left( \frac{\partial^{2}}{\partial x^{2}} + \varepsilon_{3} \frac{\partial^{2}}{\partial z^{2}} \right) \end{bmatrix}.$$
(18)

Equation (17) is a homogeneous set of differential equations in u, w, C, T. The general solution by the operator theory as follows

$$u = A_{i1}F,$$
  $w = A_{i2}F,$   $C = A_{i3}F,$   $T = A_{i4}F,$   $(i = 1, 2, 3, 4)$  (19)

where  $A_{ij}$  are algebraic cofactors of the matrix D, of which the determinant is

$$\left|D\right| = \left(a^* \frac{\partial^6}{\partial z^6} + b^* \frac{\partial^6}{\partial x^2 \partial z^4} + c^* \frac{\partial^6}{\partial x^4 \partial z^2} + d^* \frac{\partial^6}{\partial x^6}\right) \times \left(\frac{\partial^2}{\partial x^2} + \varepsilon_3 \frac{\partial^2}{\partial z^2}\right),\tag{20}$$

where

$$a^{*} = \delta_{2}(\varepsilon_{1}q_{4}^{*} - \delta_{4}q_{6}^{*}), \quad b^{*} = \delta_{1}(\varepsilon_{1}q_{4}^{*} - \delta_{4}q_{6}^{*}) - \delta_{2}(\delta_{2}q_{6}^{*} + \delta_{4}q_{5}^{*}) + \delta_{2}(\varepsilon_{1}q_{2}^{*} + \delta_{3}q_{6}^{*}) - q_{7}^{*}(\delta_{4} + \delta_{2}\varepsilon_{1}) + \delta_{3}q_{4}^{*},$$

$$c^{*} = \delta_{1}(\varepsilon_{1}q_{2}^{*} - \delta_{4}q_{5}^{*}) - \delta_{2}(\delta_{1}q_{6}^{*} + \delta_{2}q_{5}^{*}) + \delta_{2}(\delta_{3}q_{5}^{*} - \varepsilon_{1}q_{1}^{*}) + \delta_{3}q_{2}^{*} - \delta_{4}q_{1}^{*} - \delta_{2}q_{7}^{*}, \quad d = -\delta_{2}(\delta_{1}q_{5}^{*} + q_{1}^{*}).$$

The function F in equation (19) satisfies the following homogeneous equation:

$$\left|D\right|F=0.\tag{21}$$

82

As known from the generalized Almansi theorem (Ding et al. [10]), the function F can be expressed in terms of four harmonic functions:

(i) 
$$F = F_1 + F_2 + F_3 + F_4$$
 for distinct  $s_j$   $(j = 1, 2, 3, 4);$  (25a)

(ii) 
$$F = F_1 + F_2 + F_3 + zF_4$$
 for  $s_1 \neq s_2 \neq s_3 = s_4$ ; (25b)

(iii) 
$$F = F_1 + F_2 + zF_3 + z^2F_4$$
 for  $s_1 \neq s_2 = s_3 = s_4$ ; (25c)

(iv) 
$$F = F_1 + zF_2 + z^2F_3 + z^3F_4$$
 for  $s_1 = s_2 = s_3 = s_4$ . (25d)

Here  $F_j$  (j = 1, 2, 3, 4) satisfies the following harmonic equation:

$$\left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial z_j^2}\right) F_j = 0 \qquad (j = 1, 2, 3, 4).$$
(26)

The general solution for the case of distinct roots, can be derived as follows

$$u = \sum_{j=1}^{4} p_{1j} \frac{\partial^5 F_j}{\partial x \partial z_j^4}, \qquad w = \sum_{j=1}^{4} s_j p_{2j} \frac{\partial^5 F_j}{\partial z_j^5}, \qquad C = \sum_{j=1}^{4} p_{3j} \frac{\partial 6 F_j}{\partial z_j^6}, \qquad T = \sum_{j=1}^{4} p_{44} \frac{\partial^6 F_4}{\partial z_4^6}.$$
(27)

In the similar way general solution for the other three cases can be derived. Equation (23) can be further simplified by taking

$$p_{1j}\frac{\partial^4 F_j}{\partial z_j^4} = \psi_j. \tag{28}$$

Using the formula (23) in equation (22) gives

$$u = \sum_{j=1}^{4} \frac{\partial \psi_j}{\partial x}, \qquad w = \sum_{j=1}^{4} s_j P_{1j} \frac{\partial \psi_j}{\partial z_j}, \qquad C = \sum_{j=1}^{4} P_{2j} \frac{\partial^2 \psi_j}{\partial z_j^2}, \qquad T = \sum_{j=1}^{4} P_{34} \frac{\partial^2 \psi_4}{\partial z_4^2}, \tag{29}$$

where

$$P_{1j} = p_{2j} / p_{1j}, \quad P_{2j} = p_{3j} / p_{1j}, \quad P_{34} = p_{44} / p_{14}.$$
 (30)

The function  $\psi_i$  satisfies the harmonic equations:

$$\left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial z_j^2}\right)\psi_j = 0 \qquad j = 1, 2, 3, 4.$$
(31)

Making use of Eqs. (9), (11) and (12) in equation (1) and after suppressing the primes, with the aid of Eq. (29), we obtain:

Cartesian coordinate (x, z) and the surface z = 0 is free, impermeable boundary and thermally insulated. The general solution given by equations (29) and (35) is derived in this section.

For future reference, following notations are introduced:



Fig. 1. Geometry of the problem.

Green's functions in the semi-infinite plane are assumed of the following form:

$$\psi_{j} = A_{j} \left[ \frac{1}{2} (\overline{z}_{jj}^{2} - x^{2}) \left( \log \overline{r}_{jj} - \frac{3}{2} \right) - x \overline{z}_{jj} \tan^{-1}(\frac{x}{\overline{z}_{jj}}) \right] + \sum_{k=1}^{4} A_{jk} \left[ \frac{1}{2} (z_{jk}^{2} - x^{2}) \left( \log r_{jk} - \frac{3}{2} \right) - x z_{jk} \tan^{-1}(\frac{x}{z_{jk}}) \right],$$
(38)

where  $A_j$  and  $A_{jk}$  (j, k = 1, 2, 3, 4) are twenty constant to be determined. The boundary conditions on the surface (z = 0) are in the form of

$$\sigma_{zz} = \sigma_{zx} = 0, \qquad \qquad \frac{\partial C}{\partial z} = 0, \qquad \qquad \frac{\partial T}{\partial z} = 0.$$
 (39)

Substituting the equation (38) in equations (29) and (35) gives the expressions for components of displacement, mass concentration, temperature distribution and stress components as follows:

$$u = -\sum_{j=1}^{4} A_j \left[ x(\log \bar{r}_{jj} - 1) + \bar{z}_{jj} \tan^{-1} \frac{x}{\bar{z}_{jj}} \right] - \sum_{j=1}^{4} \sum_{k=1}^{4} A_{jk} \left[ x(\log r_{jk} - 1) + z_{jk} \tan^{-1} \frac{x}{z_{jk}} \right],$$
(40a)

86

When the mechanical, concentration and thermal equilibrium for a rectangle of  $\overline{a}_1 \le z \le \overline{a}_2$  $(0 < \overline{a}_1 < h < \overline{a}_2)$  and  $-\overline{b} \le x \le \overline{b}$  are considered (Fig. 1), three equations can be obtained:

$$\int_{-\overline{b}}^{\overline{b}} [\sigma_{zz}(x,\overline{a}_2) - \sigma_{zz}(x,\overline{a}_1)] dx + \int_{\overline{a}_1}^{\overline{a}_2} [\sigma_{zx}(\overline{b},z) - \sigma_{zx}(-\overline{b},z)] dz = 0,$$
(45a)

$$-\varepsilon_{3}\int_{-\overline{b}}^{\overline{b}} \left[\frac{\partial T}{\partial z}(x,\overline{a}_{2}) - \frac{\partial T}{\partial z}(x,\overline{a}_{1})\right] dx - \int_{\overline{a}_{1}}^{\overline{a}_{2}} \left[\frac{\partial T}{\partial x}(\overline{b},z) - \frac{\partial T}{\partial x}(-\overline{b},z)\right] dz = H,$$
(45b)

$$\int_{-\overline{b}}^{\overline{b}} \left[ \frac{\partial C}{\partial z}(x,\overline{a}_2) - \frac{\partial C}{\partial z}(x,\overline{a}_1) \right] dx + \int_{\overline{a}_1}^{\overline{a}_2} \left[ \frac{\partial C}{\partial x}(\overline{b},z) - \frac{\partial C}{\partial x}(-\overline{b},z) \right] dz = 0.$$
(45c)

Some useful integrals are given as follows:

$$\int \log \bar{r}_{jj} dx = x (\log \bar{r}_{jj} - 1) + \bar{z}_{jj} \tan^{-1}(\frac{x}{\bar{z}_{jj}}),$$
(46a)

$$\int \log r_{jk} dx = x (\log r_{jk} - 1) + z_{jk} \tan^{-1}(\frac{x}{z_{jk}}),$$
(46b)

$$\int \frac{\partial T}{\partial z} dx = s_4 P_{34} \left( A_4 \tan^{-1} \frac{x}{\bar{z}_{44}} + \sum_{k=1}^4 A_{4k} \tan^{-1} \frac{x}{\bar{z}_{4k}} \right), \tag{46c}$$

$$\int \frac{\partial T}{\partial x} dz = -\frac{P_{34}}{s_4} \left( A_4 \tan^{-1} \frac{x}{\bar{z}_{44}} + \sum_{k=1}^4 A_4 \tan^{-1} \frac{x}{z_{4k}} \right), \tag{46d}$$

$$\int \frac{\partial C}{\partial z} dx = A_j s_j P_{2j} \tan^{-1} \frac{x}{\bar{z}_{jj}} + \sum_{k=1}^4 A_{jk} s_j P_{2j} \tan^{-1} \frac{x}{z_{jk}},$$
(46e)

$$\int \frac{\partial C}{\partial x} dz = -\frac{A_j}{s_j} P_{2j} \tan^{-1} \frac{x}{\bar{z}_{jj}} - \sum_{k=1}^4 \frac{A_{jk}}{s_j} P_{2j} \tan^{-1} \frac{x}{z_{jk}}.$$
(46f)

It is noticed that the integrals (46d) and (46f) are not continuous at z = h, thus following expression should be used

$$\int_{\overline{a}_{1}}^{\overline{a}_{2}} \frac{\partial T}{\partial x} dz = \int_{\overline{a}_{1}}^{h^{-}} \frac{\partial T}{\partial x} dz + \int_{h^{+}}^{\overline{a}_{2}} \frac{\partial T}{\partial x} dz,$$
(47a)

$$= 2(s_j^2 - 1) \left[ \tan^{-1} \frac{\overline{b}}{s_j \overline{a}_2 + s_j h} - \tan^{-1} \frac{\overline{b}}{s_j \overline{a}_1 + s_j h} \right].$$

Substituting equation (40d) into equation (45b) with the aid of  $s_4 = \sqrt{K_1 / K_3}$  and integrals (46c) and (46d) and (47a), yields

$$A_4 I_5 + \sum_{k=1}^4 A_{4k} I_6 = \frac{H}{P_{34}\sqrt{K_3/K_1}},$$
(51)

where

$$I_{5} = -\left[\left(\tan^{-1}\left(\frac{x}{\overline{z}_{44}}\right)\right)_{z=\overline{a}_{1}}^{z=\overline{a}_{2}}\right]_{x=-\overline{b}}^{x=\overline{b}} - \left[\left(\tan^{-1}\left(\frac{x}{\overline{z}_{44}}\right)\right)_{x=-\overline{b}}^{x=\overline{b}}\right]_{z=\overline{a}_{1}}^{z=h^{-}} + \left[\left(\tan^{-1}\left(\frac{x}{\overline{z}_{44}}\right)\right)_{x=-\overline{b}}^{x=\overline{b}}\right]_{z=h^{+}}^{z=\overline{a}_{2}} = -2\pi, \quad (52a)$$

$$I_{6} = \left[ \left( \tan^{-1}(\frac{x}{z_{4k}}) \right)_{x=-\bar{b}}^{x=\bar{b}} \right]_{z=\bar{a}_{1}}^{z=\bar{a}_{2}} - \left[ \left( \tan^{-1}(\frac{x}{z_{4k}}) \right)_{z=\bar{a}_{1}}^{z=\bar{a}_{2}} \right]_{x=-\bar{b}}^{x=\bar{b}} = 0.$$
(52b)

From equations (51) and (52), we obtain

$$A_4 = -\frac{H}{2\pi P_{34}\sqrt{K_3/K_1}}.$$
(53)

Equation (37) at the surface z = 0 gives

$$z_{j} = 0, h_{k} = s_{k}h, z_{jk} = h_{k},$$

$$r_{jk} = \sqrt{x^{2} + h_{k}^{2}}, \bar{z}_{jk} = -h_{k}, \bar{r}_{jk} = \sqrt{x^{2} + h_{k}^{2}}.$$
(54)

Substituting equations (40c), (40d), (40f) and (40g) into equation (39) with the aid of  $s_4 = \sqrt{K_1/K_3}$  and equation (54), yields

$$-s_{j}w_{1j}A_{j} + \sum_{k=1}^{4} s_{k}w_{1k}A_{kj} = 0,$$
(55)

$$w_{1j}A_j + \sum_{k=1}^4 w_{1k}A_{kj} = 0,$$
(56)

$$A_4 - A_{44} = 0, (57)$$

90

$$w = \sum_{j=1}^{3} s_j P_{1j} A_j \left[ z_j (\log r_j - 1) - x \tan^{-1} \frac{x}{z_j} \right],$$
(60b)

$$T = A_4 P_{34} \log r_4, \tag{60c}$$

$$\sigma_{xx} = -\sum_{j=1}^{3} s_{j}^{2} w_{1j} A_{j} \log r_{j},$$
(60d)

$$\sigma_{zz} = \sum_{j=1}^{3} w_{1j} A_j \log r_j,$$
(60e)

$$\sigma_{zx} = -\sum_{j=1}^{3} s_j w_{1j} A_j \tan^{-1} \frac{x}{z_j}.$$
 (60f)

The above results are similar to the results obtained by Hou et al. [13].

## 6. Numerical results and discussion

For the purpose of numerical computation, we take the following values of the relevant parameters as:

$$\begin{array}{ll} \mathbf{c}_{11} = 18.78 \times 10^{10} \ \mathrm{Kg} \ \mathrm{m}^{-1} \mathrm{s}^{-2}, & \mathbf{c}_{13} = 8.0 \times 10^{10} \ \mathrm{Kg} \ \mathrm{m}^{-1} \mathrm{s}^{-2}, & \mathbf{c}_{33} = 10.2 \times 10^{10} \ \mathrm{Kg} \ \mathrm{m}^{-1} \mathrm{s}^{-2}, \\ \mathbf{c}_{55} = 10.06 \times 10^{10} \ \mathrm{Kg} \ \mathrm{m}^{-1} \mathrm{s}^{-2}, & T_0 = 0.293 \times 10^3 \ \mathrm{K}, & \alpha_1 = 2.98 \times 10^{-5} \ \mathrm{K}^{-1}, & \alpha_3 = 2.4 \times 10^{-5} \ \mathrm{K}^{-1}, \\ \alpha_{1c} = 1.1 \times 10^{-4} \ m^3 \ \mathrm{Kg}^{-1}, & K_1 = 0.12 \times 10^3 \ \mathrm{W} \ m^{-1} \ \mathrm{K}^{-1}, & K_3 = 0.33 \times 10^3 \ \mathrm{W} \ m^{-1} \ \mathrm{K}^{-1}, \\ a = 1.4 \times 10^4 \ m^2 \ \mathrm{s}^{-2} \ \mathrm{K}^{-1}, & b = 9 \times 10^5 \ \mathrm{Kg}^{-1} \ m^5 \ \mathrm{s}^{-2}, & \alpha_1^* = 0.95 \times 10^{-8} \ m^{-3} \ \mathrm{Kg}, \\ \alpha_3^* = 0.90 \times 10^{-8} \ m^{-3} \ \mathrm{Kg}, & H_0 = 0.38, & \mu_0 = 1 \\ a_1 = c_{11} \alpha_1 + c_{13} \alpha_3, & a_3 = c_{13} \alpha_1 + c_{33} \alpha_3, & b_1 = c_{11} \alpha_{1c} + c_{13} \alpha_{3c}, & b_3 = c_{13} \alpha_{1c} + c_{33} \alpha_{3c}. \end{array}$$

Figures 2-5 depict the variation of horizontal displacement (u), vertical displacement (w), temperature distribution (T) and mass concentration (C) w.r.t x. The solid line and dotted line correspond to thermoelastic diffusion (TD) and centre symbol on these lines correspond to magnetothermoelastic diffusion (MTD).

Figure 2 depicts the variation of horizontal displacement u with x and it indicates that the values of u increases for all values of x in both cases TD and MTD. It is noticed that the values of u in case of TD remain more (in comparison with MTD). Figure 3 shows that the values of vertical displacement w slightly decrease for smaller values of x, whereas for higher values of x the values of w oscillates. It is evident that the values of w in case of MTD remain more for smaller values of x although for higher values of x reverse behavior occurs. Figure 4 exhibits the variation of temperature distribution T with x and it indicates that the values of T slightly increases for smaller values of x whereas for higher values of x, the values of T increases monotonically. It is noticed that the values of T in case of MTD remain more (in comparison with MTD) for higher values of x. Figure 5 shows that the values of mass concentration C slightly decrease for smaller values of x, although for higher values of x the values of C increase. It is evident that the values of x, although for higher values of x the values of C increase. It is evident that the values of C in case of TD remain more (in comparison with MTD) for higher values of x.





**Fig. 5.** Variation of mass concentration w.r.t. *x*.

# 7. Concluding remarks

The Green's functions for two-dimensional in orthotropic magnetothermoelastic diffusion material have been derived. By virtue of the two-dimensional general solution of orthotropic magnetothermoelastic diffusion material, the Green functions for a steady line heat source on the surface of a semi-infinite plane are obtained by four newly introduced harmonic functions  $\psi_i$  (j = 1, 2, 3, 4). The general expression for components of displacement, stress, mass

concentration and temperature change are expressed in terms of elementary functions. Since all the components are expressed in terms of elementary functions, it is convenient to use them. From the present investigation, some special cases of interest are also deduced and compared with the previous results obtained. The components of displacement, mass concentration and temperature distribution are computed numerically and depicted graphically to depict the effect of magnetic.

#### References

- [1] I. Freedholm // Acta Mathem. 23 (1900) 1.
- [2] I.M. Lifshitz, L.N. Rozentsveig // Zhurnal Eksperimental'noi i Teioretical Fiziki, 17 (1947) 783.
- [3] H.A. Elliott // Proc. Cambridge Philos. Soc. 44 (1948) 522.
- [4] E. Kröner // Z. Phys. **136** (1953) 402.
- [5] J.L. Synge, *The Hypercircle in Mathematical Physics* (Cambridge University Press, London, UK, 1957).
- [6] L. Lejček // Czech. J. Phys. B 19 (1969) 799.
- [7] Y.C. Pan, T.W. Chou // J. Appl. Mech. 43 (1976) 608.
- [8] E. Pan, F.G. Yuan // Int. J. Solid Struct. 37 (2000) 5329.
- [9] B. Sharma // J. Appl. Mech. 23 (1958) 86.
- [10] H.J. Ding // Int. J. Solid Struct. 33 (1996) 2283.
- [11] P.F. Hou, A.Y.T. Leung, C.P. Chen // Z. Angew. Math. Mech. 1 (2008) 33.
- [12] P.F. Hou, L. Wang, T. Yi // Appl. Math. Model. 33 (2009) 1674.
- [13] P.F. Hou, H. Sha, C.P. Chen // Engineer. Anal. Bound. Elem. 45 (2008) 392.
- [14] S. Kaloski, W. Nowacki // Bull. Acad. Polon Sci. Sr.Sci.Techn. 18 (1970) 155.
- [15] M.I.A. Othman, Y. Song // Appl. Math. Model. 32 (2008) 483.
- [16] P.F. Hou, T. Yi, L. Wang // J. Thermal Stress. 31 (2008) 807.
- [17] W. Nowacki // Bulletin of Polish Academy of Sciences. Science and Tech. 22 (1974) 55.
- [18] W. Nowacki // Bulletin of Polish Academy of Sciences. Science and Tech. 22 (1974) 129.
- [19] W. Nowacki // Bulletin of Polish Academy of Sciences. Science and Tech. 22 (1974) 275.
- [20] W. Nowacki // Proc. Vib. Prob. 15 (1974) 105.
- [21] H.H. Sherief, H. Saleh // Int. J. of Solid and Struct. 42 (2005) 4484.
- [22] R. Kumar, V. Chawla // Int. Commun. Heat Mass Trans. 38 (2011) 456.
- [23] R. Kumar, V. Chawla // Engineering Analysis with Boundary Elements 36 (2012) 1272.
- [24] R. Kumar, V. Chawla // Theoretical and Applied Mechanics 39 (2012) 165.
- [25] M.A. Ezzat // Int. J. Eng. Sci. 35 (1997) 741.
- [26] A.C. Eringen, Foundations and Solids, Microcontinuum Field Theories (Springer-Verlag, New York, 1999).